## PLTW Engineering

## PLTW Engineering Formula Sheet 2014

### 1.0 Statistics

## Mean

$\mu=\frac{\sum x_{i}}{N} \quad$ (1.1a) $\quad \bar{x}=\frac{\sum x_{i}}{n}$ (1.1b)
$\mu=$ population mean
$\overline{\mathrm{x}}$ = sample mean
$\Sigma x_{i}=$ sum of all data values ( $x_{1}, x_{2}, x_{3}, \ldots$ )
$\mathrm{N}=$ size of population
$\mathrm{n}=$ size of sample

## Median

Place data in ascending order.
If N is odd, median = central value
If $N$ is even, median = mean of two central values
$\mathrm{N}=$ size of population

## Range (1.5)

Range $=\mathrm{x}_{\text {max }}-\mathrm{x}_{\text {min }}$
$x_{\text {max }}=$ maximum data value
$\mathrm{x}_{\text {min }}=$ minimum data value

## Mode

Place data in ascending order.
Mode = most frequently occurring value
If two values occur with maximum frequency the data set is bimodal.
If three or more values occur with maximum frequency the data set is multi-modal.

## Standard Deviation

$\sigma=\sqrt{\frac{\sum\left(\mathrm{x}_{\mathrm{i}}-\mu\right)^{2}}{\mathrm{~N}}}$
(Population)
(1.5a)
$\mathrm{s}=\sqrt{\frac{\sum\left(\mathrm{x}_{\mathrm{i}}-\overline{\mathrm{x}}\right)^{2}}{\mathrm{n}-1}}$
(Sample)
(1.5b)
$\sigma=$ population standard deviation
$\mathrm{s}=$ sample standard deviation
$\mathrm{x}_{\mathrm{i}}=$ individual data value ( $\mathrm{x}_{1}, \mathrm{x}_{2}, \mathrm{x}_{3}, \ldots$ )
$\mu=$ population mean
$\overline{\mathrm{x}}$ = sample mean
$\mathrm{N}=$ size of population
$\mathrm{n}=$ size of sample

### 2.0 Probability

## Frequency

$f_{x}=\frac{n_{x}}{n}$

## $f_{x}=$ relative frequency of outcome $x$

$\mathrm{n}_{\mathrm{x}}=$ number of events with outcome x
$\mathrm{n}=$ total number of events

## Binomial Probability (order doesn't matter)

$P_{k}=\frac{n!\left(p^{k}\right)\left(q^{n-k}\right)}{k!(n-k)!}$
$P_{k}=$ binomial probability of $k$ successes in $n$ trials
$\mathrm{p}=$ probability of a success
$q=1-p=$ probability of failure
$\mathrm{k}=$ number of successes
$\mathrm{n}=$ number of trials

## Independent Events

$\mathrm{P}(\mathrm{A}$ and B and C$)=\mathrm{P}_{\mathrm{A}} \mathrm{P}_{\mathrm{B}} \mathrm{P}_{\mathrm{C}}$
$P(A$ and $B$ and $C)=$ probability of independent
events $A$ and $B$ and $C$ occurring in sequence
$P_{A}=$ probability of event $A$

## Mutually Exclusive Events

$P(A$ or $B)=P_{A}+P_{B}$
$P(A$ or $B)=$ probability of either mutually exclusive event $A$ or $B$ occurring in a trial
$P_{A}=$ probability of event $A$

## Conditional Probability

$P(A \mid D)=\frac{P(A) \cdot P(D \mid A)}{P(A) \cdot P(D \mid A)+P(\sim A) \cdot P(D \mid \sim A)}$
$P(A \mid D)=$ probability of event $A$ given event $D$
$P(A)=$ probability of event $A$ occurring
$P(\sim A)=$ probability of event $A$ not occurring
$P(D \mid \sim A)=$ probability of event $D$ given event $A$ did not occur
3.0 Plane Geometry


## Right Triangle

$c^{2}=a^{2}+b^{2}$
(3.4)
$\sin \theta=\frac{a}{c}$
(3.5)
$\cos \theta=\frac{b}{c}$
(3.6)
$\tan \theta=\frac{\mathrm{a}}{\mathrm{b}}$
(3.7)
a

4.0 Solid Geometry

## Cube

Volume $=s^{3}$
(4.1)

Surface Area $=6 s^{2}$
(4.2)


## Rectangular Prism

Volume $=w d h$
Surface Area $=2(w d+w h+d h)$


## Right Circular Cone

Volume $=\frac{\pi r^{2} n}{3}$
Surface Area $=\pi r \sqrt{r^{2}+h^{2}}$
(4.6)


## Triangle (3.6)

Area $=1 / 2 \mathrm{bh}$
$a^{2}=b^{2}+c^{2}-2 b c \cdot \cos \angle A$
$b^{2}=a^{2}+c^{2}-2 a c \cdot \cos \angle B$
(3.12)
$c^{2}=a^{2}+b^{2}-2 a b \cdot \cos \angle C$
(3.13)
(3.11)
(3.14)

## Rectangle

Perimeter $=2 \mathrm{a}+2 \mathrm{~b}$ (3.9)
Area $=\mathrm{ab}$
(3.10)

Regular Polygons
Area $=\mathrm{n} \frac{\mathrm{s}\left(\frac{1}{2} \mathrm{f}\right)}{2}=\frac{\mathrm{ns}^{2}}{4 \tan \left(\frac{180}{\mathrm{n}}\right)}$

$\mathrm{n}=$ number of sides

## Trapezoid

Area $=1 / 2(a+b) h$


## Sphere

Volume $=\frac{4}{3} \pi r^{3}$
(4.8)

Surface Area $=4 \pi r^{2}$
(4.9)


| Cylinder |  |  |  |
| :--- | :--- | :--- | :--- |
| Volume $=\pi r^{2} h$ | (4.10) |  |  |
| Surface Area $=2 \pi r h+2 \pi r^{2}$ | (4.11) |  |  |


| Irregular Prism |  | (4.12) |
| :--- | :--- | :--- |
| Volume $=$ Ah |  |  |
| A = area of base |  |  |

### 5.0 Constants

$\mathrm{g}=9.8 \mathrm{~m} / \mathrm{s}^{2}=32.27 \mathrm{ft} / \mathrm{s}^{2}$
$\mathrm{G}=6.67 \times 10^{-11} \mathrm{~m}^{3} / \mathrm{kg} \cdot \mathrm{s}^{2}$
$\pi=3.14159$

### 6.0 Conversions



### 8.0 SI Prefixes

| Numbers Less Than One |  |  |
| :---: | :---: | :---: |
| Power of 10 | Prefix | Abbreviation |
| $10^{-1}$ | deci- | d |
| $10^{-2}$ | centi- | c |
| $10^{-3}$ | milli- | m |
| $10^{-6}$ | micro- | $\boldsymbol{\mu}$ |
| $10^{-9}$ | nano- | n |
| $10^{-12}$ | pico- | p |
| $10^{-15}$ | femto- | f |
| $10^{-18}$ | atto- | a |
| $10^{-21}$ | zepto- | z |
| $10^{-24}$ | yocto- | y |


| Numbers Greater Than One |  |  |
| :---: | :---: | :---: |
| Power of 10 | Prefix | Abbreviation |
| $10^{1}$ | deca- | da |
| $10^{2}$ | hecto- | h |
| $10^{3}$ | kilo- | k |
| $10^{6}$ | Mega- | M |
| $10^{9}$ | Giga- | G |
| $10^{12}$ | Tera- | T |
| $10^{15}$ | Peta- | P |
| $10^{18}$ | Exa- | E |
| $10^{21}$ | Zetta- | Z |
| $10^{24}$ | Yotta- | Y |

### 9.0 Equations

| Mass and Weight |  |
| :---: | :---: |
| $\mathrm{m}=\mathrm{VD}_{\mathrm{m}}$ | (9.1) |
| $\mathrm{W}=\mathrm{mg}$ | (9.2) |
| $\mathrm{W}=\mathrm{VD}_{\mathrm{w}}$ | (9.3) |
| $\mathrm{V}=$ volum <br> $\mathrm{D}_{\mathrm{m}}=$ mas <br> $\mathrm{m}=$ mass <br> $D_{w}=$ weig <br> W = weigh <br> $\mathrm{g}=$ accele | sity <br> sity <br> due |

## Temperature

$\mathrm{T}_{\mathrm{K}}=\mathrm{T}_{\mathrm{C}}+273$
$\mathrm{T}_{\mathrm{R}}=\mathrm{T}_{\mathrm{F}}+460$
$\mathrm{T}_{\mathrm{F}}=\frac{9}{5} \mathrm{~T}_{\mathrm{c}}+32$
(9.4)
(9.5)
(9.6)
$\mathrm{T}_{\mathrm{K}}=$ temperature in Kelvin
$\mathrm{T}_{\mathrm{C}}=$ temperature in Celsius
$\mathrm{T}_{\mathrm{R}}=$ temperature in Rankin
$T_{F}=$ temperature in Fahrenheit

## Force and Moment

$\mathrm{F}=\mathrm{ma} \quad$ (9.7a) $\quad \mathrm{M}=\mathrm{Fd}_{\perp} \quad$ (9.7b)
$\mathrm{F}=$ force
$\mathrm{m}=$ mass
$\mathrm{a}=$ acceleration
$\mathrm{M}=$ moment
$\mathrm{d}_{\perp}=$ perpendicular distance

## Equations of Static Equilibrium

$\Sigma F_{x}=0 \quad \Sigma F_{y}=0 \quad \Sigma M_{P}=0$
(9.8)
$F_{x}=$ force in the $x$-direction
$\mathrm{F}_{\mathrm{y}}=$ force in the y -direction
$\mathrm{M}_{\mathrm{P}}=$ moment about point P

### 9.0 Equations (Continued)

| Energy: Work |
| :--- |
| $\mathrm{W}=\mathrm{F}_{\\| \mid} \cdot \mathbf{d}$ |
| $\mathrm{W}=$ work |
| $\mathrm{F}_{\\|}=$force parallel to direction of |
| displacement |
| $\mathbf{d}=$ displacement |

## Power

$P=\frac{E}{t}=\frac{W}{t}$
$P=\tau \omega$
$\mathrm{P}=$ power
$\mathrm{E}=$ energy
W = work
t = time
$\tau=$ torque
$\omega=$ angular velocity

## Efficiency

Efficiency (\%) $=\frac{P_{\text {out }}}{P_{\text {in }}} \cdot 100 \% ~(9.12)$
$\mathrm{P}_{\text {out }}=$ useful power output
$P_{\text {in }}=$ total power input

| Energy: Potential |
| :--- |
| $\mathrm{U}=\mathrm{mgh}$ |
| $\mathrm{U}=$ potential energy |
| $\mathrm{m}=$ mass |
| $\mathrm{g}=$ acceleration due to gravity |
| $\mathrm{h}=$ height |

## Energy: Kinetic

$K=\frac{1}{2} m v^{2}$
$\mathrm{K}=$ kinetic energy
$\mathrm{m}=$ mass
$\mathrm{v}=$ velocity

## Energy: Thermal

$\Delta Q=m c \Delta T$
(9.15)
$\Delta Q=$ change in thermal energy
$\mathrm{m}=$ mass
$\mathrm{c}=$ specific heat
$\Delta T=$ change in temperature

## Fluid Mechanics

$p=\frac{F}{A}$
$\frac{\mathrm{p}_{1}}{\mathrm{~T}_{1}}=\frac{\mathrm{p}_{2}}{\mathrm{~T}_{2}} \quad$ (Gay-Lussanc's Law)
$\mathrm{p}_{1} \mathrm{~V}_{1}=\mathrm{p}_{2} \mathrm{~V}_{2}$ (Boyle's Law)
$Q=A v$
$\mathrm{A}_{1} \mathrm{v}_{1}=\mathrm{A}_{2} \mathrm{v}_{2}$
absolute pressure = gauge pressure

+ atmospheric pressure (9.23)
$p=$ absolute pressure
$F=$ force
A = area
$\mathrm{V}=$ volume
$\mathrm{T}=$ absolute temperature
$Q$ = flow rate
v = flow velocity
$\mathrm{P}=$ power

| Mechanics |  |
| :---: | :---: |
| $\overline{\mathrm{S}}=\frac{\mathrm{d}}{\mathrm{t}}$ | (9.24) |
| $\overline{\mathbf{v}}=\frac{\Delta \mathbf{d}}{\Delta \mathrm{t}}$ | (9.25) |
| $a=\frac{v_{f}-v_{i}}{t}$ | (9.26) |
| $X=\frac{\mathrm{v}^{2} \sin (2 \theta)}{-\mathrm{g}}$ | (9.27) |
| $v=v_{i}+$ at | (9.28) |
| $d=d_{i}+v_{i} t+1 / 2 a t^{2}$ | (9.29) |
| $\mathrm{v}^{2}=\mathrm{v}_{\mathrm{i}}^{2}+2 \mathrm{a}\left(\mathrm{d}-\mathrm{d}_{\mathrm{i}}\right)$ | (9.30) |
| $\boldsymbol{\tau}=\mathrm{dF} \sin \theta$ | (9.31) |
| $\overline{\mathrm{s}}$ = average speed |  |
| $\overline{\mathbf{v}}=$ average velocity |  |
| $v=$ velocity |  |
| $\mathrm{v}_{\mathrm{i}}=$ initial velocity ( $\mathrm{t}=0$ ) |  |
| $\mathrm{a}=$ acceleration |  |
| $\mathrm{X}=$ range |  |
| $\mathrm{t}=$ time |  |
| $\Delta \mathbf{d}=$ change in displacement d = distance |  |
| $\mathrm{d}_{\mathrm{i}}=$ initial distance ( $\mathrm{t}=0$ ) |  |
| $\mathrm{g}=$ acceleration due to gravity |  |
| $\theta=$ angle |  |
| $\boldsymbol{\tau}=$ torque |  |
| $F=$ force |  |

## Electricity

## Ohm's Law

$\mathrm{V}=\mathrm{IR}$
$\mathrm{P}=\mathrm{IV}$
$R_{T}$ (series) $=R_{1}+R_{2}+\cdots+R_{n}$
$\mathrm{R}_{\mathrm{T}}($ parallel $)=\frac{1}{\frac{1}{R_{1}+\frac{1}{R_{2}}+\cdots+\frac{1}{R_{n}}}}$

## Kirchhoff's Current Law

$I_{T}=I_{1}+I_{2}+\cdots+I_{n}$

$$
\begin{equation*}
\text { or } \mathrm{I}_{\mathrm{T}}=\sum_{\mathrm{k}=1}^{\mathrm{n}} \mathrm{I}_{\mathrm{k}} \tag{9.36}
\end{equation*}
$$

## Kirchhoff's Voltage Law

$$
V_{T}=V_{1}+V_{2}+\cdots+V_{n}
$$

$$
\begin{equation*}
\text { or } \quad V_{T}=\sum_{k=1}^{n} V_{k} \tag{9.37}
\end{equation*}
$$

$\mathrm{V}=$ voltage
$\mathrm{V}_{\mathrm{T}}=$ total voltage
I = current
$\mathrm{I}_{\mathrm{T}}=$ total current
$R=$ resistance
$\mathrm{R}_{\mathrm{T}}=$ total resistance
$\mathrm{P}=$ power

## Thermodynamics

$P=Q^{\prime}=A U \Delta T$
$P=Q^{\prime}=\frac{\Delta Q}{\Delta t}$
$U=\frac{1}{R}=\frac{k}{L}$
$P=\frac{k A \Delta T}{L}$
$\mathrm{A}_{1} \mathrm{v}_{1}=\mathrm{A}_{2} \mathrm{v}_{2}$
$P_{\text {net }}=\sigma \operatorname{Ae}\left(T_{2}{ }^{4}-T_{1}{ }^{4}\right)$
$\mathrm{k}=\frac{\mathrm{PL}}{\mathrm{A} \Delta \mathrm{T}}$
$\mathrm{P}=$ rate of heat transfer
$Q=$ thermal energy
$A=$ area of thermal conductivity
$U=$ coefficient of heat conductivity
(U-factor)
$\Delta T=$ change in temperature
$\Delta \mathrm{t}=$ change in time
$R=$ resistance to heat flow (R-value)
$\mathrm{k}=$ thermal conductivity
$\mathrm{v}=$ velocity
$P_{\text {net }}=$ net power radiated
$\sigma=5.6696 \times 10^{-8} \frac{\mathrm{~W}}{\mathrm{~m}^{2} \cdot \mathrm{k}^{4}}$
$e=$ emissivity constant
L = thickness
$\mathrm{T}_{1}, \mathrm{~T}_{2}=$ temperature at time 1 , time 2

### 10.0 Section Properties

## Moment of Inertia

$I_{x x}=\frac{b h^{3}}{12}$
(10.1)

$I_{x x}=$ moment of inertia of a rectangular section about x axis

## Complex Shapes Centroid

$\bar{x}=\frac{\sum x_{i} A_{i}}{\sum A_{i}}$ and $\bar{y}=\frac{\sum y_{i} A_{i}}{\sum A_{i}}$
$\overline{\mathrm{x}}=\mathrm{x}$-distance to the centroid
$\bar{y}=y$-distance to the centroid
$x_{i}=x$ distance to centroid of shape $i$
$y_{i}=y$ distance to centroid of shape $i$
$A_{i}=$ Area of shape $i$

## Rectangle Centroid

$\bar{x}=\frac{b}{2}$ and $\bar{y}=\frac{h}{2}$
(10.3)


Right Triangle Centroid
$\bar{x}=\frac{b}{3}$ and $\bar{y}=\frac{h}{3}$
(10.4)


Semi-circle Centroid
$\bar{x}=r$ and $\bar{y}=\frac{4 r}{3 \pi}$
(10.5)

$\bar{x}=x$-distance to the centroid
$\overline{\mathrm{y}}=\mathrm{y}$-distance to the centroid

### 11.0 Material

## Stress (axial) <br> $\sigma=\frac{\mathrm{F}}{\mathrm{A}}$ <br> $\sigma=$ stress <br> $\mathrm{F}=$ axial force <br> $\mathrm{A}=$ cross-sectional area

## Strain (axial)

$\varepsilon=\frac{\delta}{L_{0}}$
$\varepsilon=$ strain
$\mathrm{L}_{0}=$ original length
$\delta=$ change in length

## Modulus of Elasticity

$E=\frac{\sigma}{\varepsilon}$
(11.3)
$E=\frac{\left(F_{2}-F_{1}\right) L_{0}}{\left(\delta_{2}-\delta_{1}\right) A}$
$\mathrm{E}=$ modulus of elasticity
$\sigma=$ stress
$\varepsilon=$ strain
$\mathrm{A}=$ cross-sectional area
$\mathrm{F}=$ axial force
$\delta=$ deformation

### 12.0 Structural Analysis

| Beam Formulas |  |  |  |
| :---: | :---: | :---: | :---: |
|  | Reaction <br> Moment <br> Deflection | $\begin{aligned} & R_{A}=R_{B}=\frac{P}{2} \\ & M_{\max }=\frac{\mathrm{PL}}{4} \quad \text { (at point of load) } \\ & \Delta_{\max }=\frac{\mathrm{PL}}{48 E 1} \text { (at point of load) } \end{aligned}$ | $\begin{gathered} (12.1) \\ (12.2) \\ (12.3) \end{gathered}$ |
|  | Reaction <br> Moment <br> Deflection | $\begin{aligned} & R_{A}=R_{B}=\frac{\omega L}{2} \\ & M_{\max }=\frac{\omega L^{2}}{8} \quad \text { (at center) } \\ & \Delta_{\max }=\frac{5 \omega L^{4}}{384 E I} \quad \text { (at center) } \end{aligned}$ | $\begin{aligned} & (12.4) \\ & (12.5) \\ & (12.6) \end{aligned}$ |
|  | Reaction <br> Moment <br> Deflection | $\begin{aligned} & \mathrm{R}_{\mathrm{A}}=\mathrm{R}_{\mathrm{B}}=\mathrm{P} \\ & \mathrm{M}_{\max }=\mathrm{Pa} \\ & \Delta_{\max }=\frac{\mathrm{Pa}}{24 \mathrm{Ea}}\left(3 \mathrm{aL}^{2}-4 \mathrm{a}^{2}\right) \\ & \text { (at center) } \end{aligned}$ | $\begin{aligned} & (12.7) \\ & (12.8) \\ & (12.9) \end{aligned}$ |
|  | Reaction <br> Moment <br> Deflection | $\begin{aligned} & R_{A}=\frac{P b}{L} \text { and } R_{B}=\frac{P a}{L} \\ & M_{\text {max }}=\frac{\text { Pab }}{L}(\text { at Point of Load } \\ & \Delta_{\text {max }}=\frac{\text { Pab }(a+2 b) \sqrt{3 a(a+2 b)}}{} \\ & \quad\left(\text { at } x=\sqrt{\frac{(a+2 b)}{3,}} \text { when } \mathrm{a}>\mathrm{b}\right) \end{aligned}$ | $\begin{gathered} (12.10) \\ \text { d) }(12.11) \\ (12.12) \end{gathered}$ |

## Deformation: Axial

$\delta=\frac{\mathrm{FL}_{0}}{\mathrm{AE}}$
$\delta=$ deformation
$\mathrm{F}=$ axial force
$\mathrm{L}_{0}=$ original length
A $=$ cross-sectional area
$\mathrm{E}=$ modulus of elasticity

## Truss Analysis

$\underline{\mathrm{J}}=\mathrm{M}+\mathrm{R}$
(12.14)
$J=$ number of joints
$\mathrm{M}=$ number of members
$R=$ number of reaction forces

### 13.0 Simple Machines

## Mechanical Advantage (MA)

$$
\begin{equation*}
\mathrm{IMA}=\frac{\mathrm{D}_{\mathrm{E}}}{\mathrm{D}_{\mathrm{R}}} \quad \text { (13.1) } \quad \mathrm{AMA}=\frac{\mathrm{F}_{\mathrm{R}}}{\mathrm{~F}_{\mathrm{E}}} \tag{13.2}
\end{equation*}
$$

\% Efficiency=( (AMA $) 100$
IMA = ideal mechanical advantage
AMA = actual mechanical advantage
$\mathrm{D}_{\mathrm{E}}=$ effort distance
$D_{R}=$ resistance distance
$F_{E}=$ effort force
$F_{R}=$ resistance force

## Lever

1 st
Class

2nd
Class

3rd
Class


Wheel and Axle


Effort at Wheel


## Pulley Systems

IMA = total number of strands of a single string supporting the resistance
(13.4)

IMA $=\frac{D_{E}(\text { string pulled })}{D_{R}(\text { resistance lifted })}$

## Inclined Plane

$I M A=\frac{L}{H}$


## Wedge

$I M A=\frac{L}{H}$
(13.7)


## Screw

IMA $=\frac{C}{\text { Pitch }}$
(13.8)

Pitch $=\frac{1}{\mathrm{TPI}}$
Pitch

$\mathrm{C}=$ circumference
$\mathrm{r}=$ radius
Pitch = distance between
threads
TPI = threads per inch

## Compound Machines

$M A_{\text {TOTAL }}=\left(M A_{1}\right)\left(\mathrm{MA}_{2}\right)\left(\mathrm{MA}_{3}\right) \ldots$

Gears; Sprockets with Chains; and Pulleys with Belts Ratios

$$
\begin{align*}
& \mathrm{GR}=\frac{N_{\text {out }}}{N_{\text {in }}}=\frac{d_{\text {out }}}{d_{\text {in }}}=\frac{\omega_{\text {in }}}{\omega_{\text {out }}}=\frac{\tau_{\text {out }}}{\tau_{\text {in }}}  \tag{13.11}\\
& \frac{d_{\text {out }}}{d_{\text {in }}}=\frac{\omega_{\text {in }}}{\omega_{\text {out }}}=\frac{\tau_{\text {out }}}{\tau_{\text {in }}} \text { (pulleys) } \tag{13.12}
\end{align*}
$$

Compound Gears
$\mathrm{GR}_{\text {TOTAL }}=\left(\frac{\mathrm{B}}{\mathrm{A}}\right)\left(\frac{\mathrm{D}}{\mathrm{C}}\right)$

$\mathrm{GR}=$ gear ratio
$\omega_{\text {in }}=$ angular velocity - driver
$\omega_{\text {out }}=$ angular velocity - driven
$\mathrm{N}_{\text {in }}=$ number of teeth - driver
$\mathrm{N}_{\text {out }}=$ number of teeth - driven
$\mathrm{d}_{\mathrm{in}}=$ diameter - driver
$\mathrm{d}_{\text {out }}=$ diameter - driven
$\tau_{\text {in }}=$ torque - driver
$\tau_{\text {out }}=$ torque - driven

### 14.0 Structural Design

## Steel Beam Design: Shear

$V_{a} \leq \frac{V_{n}}{\Omega_{v}}$
$V_{n}=0.6 F_{y} A_{w}$
(14.2)
$\mathrm{V}_{\mathrm{a}}=$ internal shear force
$\mathrm{V}_{\mathrm{n}}=$ nominal shear strength
$\Omega_{\mathrm{v}}=1.5=$ factor of safety for shear
$\mathrm{F}_{\mathrm{y}}=$ yield stress
$\mathrm{A}_{\mathrm{w}}=\mathrm{area}$ of web
$\frac{V_{n}}{n_{v}}=$ allowable shear strength

### 15.0 Storm Water Runoff

## Storm Water Drainage

$\mathrm{Q}=\mathrm{C}_{\mathrm{f}} \mathrm{CiA}$
$C_{C}=\frac{C_{1} A_{1}+C_{2} A_{2}+\cdots}{A_{1}+A_{2}+\cdots}$
$\mathrm{Q}=$ peak storm water runoff rate ( $\mathrm{ft}^{3} / \mathrm{s}$ )
$\mathrm{C}_{\mathrm{f}}=$ runoff coefficient adjustment factor
C = runoff coefficient
i = rainfall intensity (in./h)
A = drainage area (acres)

| Runoff Coefficient <br> Adjustment Factor |  |
| :--- | :--- |
| Return <br> Period | Cf |
| $1,2,5,10$ | 1.0 |
| 25 | 1.1 |
| 50 | 1.2 |
| 100 | 1.25 |


| Steel Beam Design: Moment |  |
| :---: | :---: |
| $\mathrm{M}_{\mathrm{a}} \leq \frac{\mathrm{M}_{\mathrm{n}}}{\Omega_{\mathrm{b}}}$ | (14.3) |
| $M_{n}=F_{y} Z_{x}$ | (14.4) |
| $\mathrm{M}_{\mathrm{a}}=$ internal bending moment |  |
| $\Omega_{b}=1.67=$ factor of safety for bending moment |  |
| $\mathrm{F}_{\mathrm{y}}=$ yield stress |  |
| $\mathrm{Z}_{\mathrm{x}}=$ plastic section modulus about neutral axis |  |
| $\frac{M_{n}}{\Omega_{b}}=$ allowable bending strength |  |


| Rational Method Runoff Coefficients |  | footing |
| :---: | :---: | :---: |
| Categorized by Surface |  |  |
| Forested | 0.059-0.2 | 16.0 Water Supply |
| Asphalt | 0.7-0.95 |  |
| Brick | 0.7-0.85 |  |
| Concrete | 0.8-0.95 | Hazen-Williams Formula |
| Shingle roof | 0.75-0.95 | $\mathrm{hf}_{\mathrm{f}}=\frac{10.44 \mathrm{LQ}}{} \mathrm{C}^{1.85} \mathrm{~d}^{4.8655}$ |
| Lawns, well drained (sandy soil) |  |  |
| Up to 2\% slope $2 \%$ to $7 \%$ slope Over 7\% slope | 0.05-0.1 |  |
|  | $0.10-0.15$ | $\begin{aligned} & \mathrm{h}_{\mathrm{f}}=\text { head loss due to friction } \\ & \text { (ft of } \mathrm{H}_{2} \mathrm{O} \text { ) } \\ & \mathrm{L}=\text { length of pipe ( } \mathrm{ft} \text { ) } \\ & \mathrm{Q}= \text { water flow rate ( } \mathrm{gpm} \text { ) } \\ & \mathrm{C}=\text { Hazen-Williams constant } \end{aligned}$ |
|  | 0.15-0.2 |  |
| Lawns, poor drainage (clay soil) |  |  |
| Up to 2\% slope 2\% to $7 \%$ slope Over 7\% slope | 0.13-0.17 |  |
|  | 0.18-0.22 |  |
|  | 0.25-0.35 |  |
| Driveways, | 0.75-0.85 | Dynamic Head |
| Categorized by Use |  | dynamic head = static head - head loss (16.2) static head = change in elevation between source and discharge |
| Farmland | 0.05-0.3 |  |
| Pasture | 0.05-0.3 |  |
| Unimproved | 0.1-0.3 |  |
| Parks | 0.1-0.25 |  |
| Cemeteries | 0.1-0.25 | 17.0 Heat Loss/Gain |
| Railroad yard | 0.2-0.40 |  |
| Playgrounds | 0.2-0.35 |  |
| Business Districts |  | Heat Loss/Gain |
| Neighborhood | 0.5-0.7 | $\mathrm{Q}^{\prime}=\mathrm{AU} \mathrm{\Delta T}$ |
| City (downtown) | 0.7-0.95 | $Q=A U \Delta T$ |
| Residential |  | $\mathrm{U}=\frac{1}{\mathrm{R}}$ |
| Single-family | 0.3-0.5 |  |
| Multi-plexes, | 0.4-0.6 | Q = thermal energy |
| Multi-plexes, | 0.6-0.75 | A = area of thermal conductivity |
| Suburban | 0.25-0.4 | $\mathrm{U}=$ coefficient of heat |
| Apartments, | 0.5-0.7 | conductivity (U-factor) |
| Industrial |  | $\Delta \mathrm{T}=$ change in temperature |
| Light | 0.5-0.8 | $R=\begin{gathered}\text { resistance to heat flow ( } R \text { - } \\ \text { value) }\end{gathered}$ |
| Heavy | 0.6-0.9 |  |

### 18.0 Hazen-Williams Constants

| Pipe Mlaterial | Typical Range | Clean, New Pipe | Typical Design <br> Value |
| :---: | :---: | :---: | :---: |
| Cast Iron and <br> Wrought Iron | $80-150$ | 130 | 100 |
| Copper, Glass <br> or Brass | $120-150$ | 140 | 130 |
| Cement lined <br> Steel or Iron | 150 | 140 |  |
| Plastic <br> PVC or ABS | $120-150$ | 140 | 130 |
| Steel, welded and <br> seamless or <br> interior riveted | $80-150$ | 140 | 100 |

### 19.0 Equivalent Length of (Generic) Fittings

| Screwed Fittings |  | Pipe Size |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1/4 | 3/8 | 1/2 | 3/4 | 1 | $11 / 4$ | $11 / 2$ | 2 | $21 / 2$ | 3 | 4 |
| Elbows | Regular 90 degree | 2.3 | 3.1 | 3.6 | 4.4 | 5.2 | 6.6 | 7.4 | 8.5 | 9.3 | 11.0 | 13.0 |
|  | Long radius 90 degree | 1.5 | 2.0 | 2.2 | 2.3 | 2.7 | 3.2 | 3.4 | 3.6 | 3.6 | 4.0 | 4.6 |
|  | Regular 45 degree | 0.3 | 0.5 | 0.7 | 0.9 | 1.3 | 1.7 | 2.1 | 2.7 | 3.2 | 4.0 | 5.5 |
| Tees | Line Flow | 0.8 | 1.2 | 1.7 | 2.4 | 3.2 | 4.6 | 5.6 | 7.7 | 9.3 | 12.0 | 17.0 |
|  | Branch Flow | 2.4 | 3.5 | 4.2 | 5.3 | 6.6 | 8.7 | 9.9 | 12.0 | 13.0 | 17.0 | 21.0 |
| Return Bends | Regular 180 degree | 2.3 | 3.1 | 3.6 | 4.4 | 5.2 | 6.6 | 7.4 | 8.5 | 9.3 | 11.0 | 13.0 |
| Valves | Globe | 21.0 | 22.0 | 22.0 | 24.0 | 29.0 | 37.0 | 42.0 | 54.0 | 62.0 | 79.0 | 110.0 |
|  | Gate | 0.3 | 0.5 | 0.6 | 0.7 | 0.8 | 1.1 | 1.2 | 1.5 | 1.7 | 1.9 | 2.5 |
|  | Angle | 12.8 | 15.0 | 15.0 | 15.0 | 17.0 | 18.0 | 18.0 | 18.0 | 18.0 | 18.0 | 18.0 |
|  | Swing Check | 7.2 | 7.3 | 8.0 | 8.8 | 11.0 | 13.0 | 15.0 | 19.0 | 22.0 | 27.0 | 38.0 |
| Strainer |  |  | 4.6 | 5.0 | 6.6 | 7.7 | 18.0 | 20.0 | 27.0 | 29.0 | 34.0 | 42.0 |


| Flanged Fittings |  | Pipe Size |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1/2 | 3/4 | 1 | $11 / 4$ | $11 / 2$ | 2 | $21 / 2$ | 3 | 4 | 5 | 6 | 8 | 10 | 12 | 14 | 16 | 18 |
| Elbows | Regular 90 degree | 0.9 | 1.2 | 1.6 | 2.1 | 2.4 | 3.1 | 3.6 | 4.4 | 5.9 | 7.3 | 8.9 | 12.0 | 14.0 | 17.0 | 18.0 | 21.0 | 23.0 |
|  | Long radius 90 degree | 1.1 | 1.3 | 1.6 | 2.0 | 2.3 | 2.7 | 2.7 | 3.4 | 4.2 | 5.0 | 5.7 | 7.0 | 8.0 | 9.0 | 9.4 | 10.0 | 11.0 |
|  | Regular 45 degree | 0.5 | 0.6 | 0.8 | 1.1 | 1.3 | 1.7 | 2.0 | 2.5 | 3.5 | 4.5 | 5.6 | 7.7 | 9.0 | 11.0 | 13.0 | 15.0 | 16.0 |
| Tees | Line Flow | 0.7 | 0.8 | 1.0 | 1.3 | 1.5 | 1.8 | 1.9 | 2.2 | 2.8 | 3.3 | 3.8 | 4.7 | 5.2 | 6.0 | 6.4 | 7.2 | 7.6 |
|  | Branch Flow | 2.0 | 2.6 | 3.3 | 4.4 | 5.2 | 6.6 | 7.5 | 9.4 | 12.0 | 15.0 | 18.0 | 24.0 | 30.0 | 34.0 | 37.0 | 43.0 | 47.0 |
| Return Bends | Regular 180 degree | 0.9 | 1.2 | 1.6 | 2.1 | 2.4 | 3.1 | 3.6 | 4.4 | 5.9 | 7.3 | 8.9 | 12.0 | 14.0 | 17.0 | 18.0 | 21.0 | 23.0 |
|  | Long radius 180 degree | 1.1 | 1.3 | 1.6 | 2.0 | 2.3 | 2.7 | 2.9 | 3.4 | 4.2 | 5.0 | 5.7 | 7.0 | 8.0 | 9.0 | 9.4 | 10.0 | 11.0 |
| Valves | Globe | 38.0 | 40.0 | 45.0 | 54.0 | 59.0 | 70.0 | 77.0 | 94.0 | 120.0 | 150.0 | 190.0. | 260.0 | 310.0 | 390.0 |  |  |  |
|  | Gate |  |  |  |  |  | 2.6 | 2.7 | 2.8 | 2.9 | 3.1 | 3.2 | 3.2 | 3.2 | 3.2 | 3.2 | 3.2 | 3.2 |
|  | Angle | 15.0 | 15.0 | 17.0 | 18.0 | 18.0 | 21.0 | 22.0 | 285.0 | 38.0 | 50.0 | 63.0 | 90.0 | 120.0 | 140.0 | 160.0 | 190.0 | 210.0 |
|  | Swing Check | 3.8 | 5.3 | 7.2 | 10.0 | 12.0 | 17.0 | 21.0 | 27.0 | 38.0 | 50.0 | 63.0 | 90.0 | 120.0 | 140.0 |  |  |  |

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PLTW Engineering Formula Sheet 2014
$\mathrm{T}=0.693\left(\mathrm{R}_{\mathrm{A}}+2 \mathrm{R}_{\mathrm{B}}\right) \mathrm{C}$
(20.1)
$f=\frac{1}{\mathrm{~T}}$
duty-cycle $=\frac{\left(R_{A}+R_{B}\right)}{\left(R_{A}+2 R_{B}\right)} \cdot 100 \%$
T = period
$f=$ frequency
$\mathrm{R}_{\mathrm{A}}=$ resistance A
$\mathrm{R}_{\mathrm{B}}=$ resistance B
$\mathrm{C}=$ capacitance

### 21.0 Boolean Algebra

| Boolean Theorems |  |
| :--- | ---: |
| $X \cdot 0=0$ | $(21.1)$ |
| $X \cdot 1=X$ | $(21.2)$ |
| $X \cdot X=X$ | $(21.3)$ |
| $X \cdot \bar{X}=0$ | $(21.4)$ |
| $X+0=X$ | $(21.5)$ |
| $X+1=1$ | $(21.6)$ |
| $X+X=X$ | $(21.7)$ |
| $X+\bar{X}=1$ | $(21.8)$ |
| $\bar{X}=X$ | $(21.9)$ |


| Commutative Law |  |
| :--- | :--- |
| $\mathrm{X} \cdot \mathrm{Y}=\mathrm{Y} \bullet \mathrm{X}$ | (21.10) |
| $\mathrm{X}+\mathrm{Y}=\mathrm{Y}+\mathrm{X}$ |  |


| Associative Law |  |
| :--- | :--- |
| $\mathrm{X}(\mathrm{YZ})=(\mathrm{XY}) \mathrm{Z}$ | (21.12) |
| $\mathrm{X}+(\mathrm{Y}+\mathrm{Z})=(\mathrm{X}+\mathrm{Y})+\mathrm{Z}$ | (21.13) |


| Consensus Theorems |  |
| :---: | :---: |
| $X+\bar{X} Y=X+Y$ | (21.16) |
| $X+\bar{X} \bar{Y}=X+\bar{Y}$ | (21.17) |
| $\bar{X}+X Y=\bar{X}+Y$ | (21.18) |
| $\bar{X}+X \bar{Y}=\bar{X}+\bar{Y}$ | (21.19) |
| DeMorgan's Theorems |  |
| $\overline{X Y}=\bar{X}+\bar{Y}$ | (21.20) |
| $\overline{X+Y}=\bar{X} \cdot \bar{Y}$ | (21.21) |

### 22.0 Speeds and Feeds

$$
\begin{equation*}
\mathrm{N}=\frac{\operatorname{cs}\left(12 \frac{\mathrm{in} . \mathrm{t}}{\mathrm{t}}\right)}{\pi \mathrm{d}} \tag{22.1}
\end{equation*}
$$

$\mathrm{f}_{\mathrm{m}}=\mathrm{f}_{\mathrm{t}} \cdot \mathrm{n}_{\mathrm{t}} \cdot \mathrm{N}$
Plunge Rate $=1 / 2 \cdot f_{m}$
$\mathrm{N}=$ spindle speed (rpm)
CS = cutting speed (in./min)
$\mathrm{d}=$ diameter (in.)
$\mathrm{f}_{\mathrm{m}}=$ feed rate (in./min)
$\mathrm{f}_{\mathrm{t}}=$ feed (in./tooth/rev)
$n_{t}=$ number of teeth

### 23.0 Aerospace

## Forces of Flight

$\mathrm{C}_{\mathrm{D}}=\frac{2 \mathrm{D}}{\mathrm{A} \mathrm{\rho v}{ }^{2}}$
$\mathrm{R}_{\mathrm{e}}=\frac{\mathrm{pvl}}{\mu}$
$C_{L}=\frac{2 L}{A \rho v^{2}}$
$\mathrm{M}=\mathrm{Fd}$
(23.4)
$\mathrm{C}_{\mathrm{L}}=$ coefficient of lift
$\mathrm{C}_{\mathrm{D}}=$ coefficient of drag
$\mathrm{L}=\mathrm{lift}$
$\mathrm{D}=\mathrm{drag}$
A = wing area
$\rho=$ density
$\mathrm{R}_{\mathrm{e}}=$ Reynolds number
$\mathrm{v}=$ velocity
$I=$ length of fluid travel
$\mu=$ fluid viscosity
$F=$ force
$\mathrm{m}=$ mass
$g=$ acceleration due to gravity
$\mathrm{M}=$ moment
$\mathrm{d}=$ moment arm (distance from datum perpendicular to F)

## Propulsion

$\mathrm{F}_{\mathrm{N}}=\mathrm{W}\left(\mathrm{v}_{\mathrm{j}}-\mathrm{v}_{\mathrm{o}}\right)$
$\mathrm{I}=\mathrm{F}_{\text {ave }} \Delta \mathrm{t}$
$\mathrm{F}_{\text {net }}=\mathrm{F}_{\text {avg }}-\mathrm{F}_{\mathrm{g}}$
$\mathrm{a}=\frac{v_{f}}{\Delta t}$
$\mathrm{F}_{\mathrm{N}}=$ net thrust
$\mathrm{W}=$ air mass flow
$\mathrm{v}_{\mathrm{o}}=$ flight velocity
$\mathrm{v}_{\mathrm{j}}=$ jet velocity
I = total impulse
$\mathrm{F}_{\text {ave }}=$ average thrust force
$\Delta t=$ change in time (thrust duration)
$\mathrm{F}_{\text {net }}=$ net force
$\mathrm{F}_{\text {avg }}=$ average force
$\mathrm{F}_{\mathrm{g}}=$ force of gravity
$\mathrm{v}_{\mathrm{f}}=$ final velocity
$\mathrm{a}=$ acceleration
$\Delta t=$ change in time (thrust duration)

NOTE: $F_{\text {ave }}$ and $F_{\text {avg }}$ are easily confused.

## Energy

$\mathrm{K}=\frac{1}{2} \mathrm{mv}^{2}$
$U=\frac{-G M m}{R}$
$E=U+K=-\frac{G M m}{2 R}$
$\mathrm{G}=6.67 \times 10^{-11} \frac{\mathrm{~m}^{3}}{\mathrm{~kg} \times \mathrm{s}^{2}}$
$\mathrm{K}=$ kinetic energy
$\mathrm{m}=$ mass
$\mathrm{v}=$ velocity
$\mathrm{U}=$ gravitational potential energy
$\mathrm{G}=$ universal gravitation constant
$\mathrm{M}=$ mass of central body
$\mathrm{m}=$ mass of orbiting object
$R=$ Distance center main body to center of orbiting object
$\mathrm{E}=$ Total Energy of an orbit

## Orbital Mechanics

$e=\sqrt{1-\frac{\mathrm{b}^{2}}{\mathrm{a}^{2}}}$
$\mathrm{T}=2 \pi \frac{\mathrm{a}^{\frac{3}{2}}}{\sqrt{\mu}}=2 \pi \frac{\mathrm{a}^{\frac{3}{2}}}{\sqrt{\mathrm{GM}}}$
$\mathrm{F}=\frac{\mathrm{GMm}}{\mathrm{r}^{2}}$
$e=$ eccentricity
$\mathrm{b}=$ semi-minor axis
a =semi-major axis
T = orbital period
a = semi-major axis
$\mu=$ gravitational parameter
F = force of gravity between two bodies
$\mathrm{G}=$ universal gravitation constant
M =mass of central body
$\mathrm{m}=$ mass of orbiting object
$r$ = distance between center of two objects

## Bernoulli's Law

$$
\begin{equation*}
\left(P_{s}+\frac{\rho v^{2}}{2}\right)_{1}=\left(P_{s}+\frac{\rho v^{2}}{2}\right)_{2} \tag{23.16}
\end{equation*}
$$

$\mathrm{P}_{\mathrm{S}}=$ static pressure
$\mathrm{v}=$ velocity
$\rho=$ density

## Atmosphere Parameters

$\mathrm{T}=15.04-0.00649 \mathrm{~h}$
$\mathrm{p}=101.29\left[\frac{(\mathrm{~T}+273.1)}{288.08}\right]^{5.256}$
$\rho=\frac{\mathrm{p}}{}{ }^{(23.17)}$
$0.2869(\mathrm{~T}+273.1)$
$\mathrm{T}=$ temperature
$\mathrm{h}=$ height
$\mathrm{p}=$ pressure
$\rho=$ density

